

Bicriterial dual control with multiple linearization

Miroslav Flidr and Miroslav Šimandl

Research Center Data, Algorithms, Decision
Department of Cybernetics
Faculty of Applied Sciences
University of West Bohemia in Pilsen
Czech Republic



Outline

1 Introduction

- Dual control
- Bicriterial approach

2 Generalized Bicriterial controller

- Goal of the paper
- Bicriterial controller for MIMO state space system
- Bicriterial controller with multiple linearization

3 Conclusion

Dual control (Feldbaum 1960)

- Arises in control problem with insufficient knowledge of parameters
- Two conflicting goals – meet control objective and improve estimation
- Optimal dual control problem – mostly cannot be solved analytically

Suboptimal solutions (Tse *et al.* 1973, Wittenmark *et al.* 1975, Millito *et al.* 1982,...)

- Augmenting the cautious control law (Bicriterial controller,...)
- Modification of criterion (e.g. IDC, ASOD,...)
- Criterion approximation (e.g. WDC, Utility cost,...)

Feasible solution - Bicriterial approach (Filatov *et al.* 1996)

- clear interpretation (two objectives \Rightarrow two criteria)
- computationally moderate (only one step ahead horizon)
- enhances the *cautious control* with a suitable *probing* signal

Bicriterial approach

Filatov, N. M., U. Keuchel and H. Unbehauen (1996). Dual control for an unstable mechanical plant. *IEEE Control Systems Magazine* **16**(4), 31–37.

- ✓ The controlled system considered SISO ARMAX
- ✓ Parameter estimation by Recursive least square method

The criteria

- Control objective criterion - leading to cautious control

$$J_k^c(u_k) = E \left\{ (\bar{y}_{k+1} - y_{k+1})^2 \mid \mathcal{I}_k \right\}, \quad \mathcal{I}_k = (u_0, \dots, u_{k-1}, y_0, \dots, y_k)$$

- Estimation objective criterion

$$J_k^e(u_k) = -E \left\{ (y_{k+1} - \hat{y}_{k+1})^2 \mid \mathcal{I}_k \right\}$$

$$u_k^* = \underset{u_k \in \Omega_k}{\operatorname{argmin}} J_k^e(u_k), \quad \Omega_k = [u_k^c - \delta_k, u_k^c + \delta_k]$$

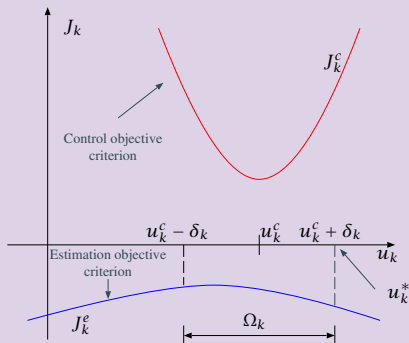
$$\delta_k = f(\mathbf{P}_k) = \eta \cdot \operatorname{tr} \mathbf{P}_k$$

Bicriterial approach

Bicriterial control law

$$u_k^* = u_k^c + \delta_k \operatorname{sign}(\omega_k)$$
$$\omega_k = J_k^e(u_k^c + \delta_k) - J_k^e(u_k^c - \delta_k)$$

Maximization of criterion $J_k^e(u_k)$ on domain Ω_k



Goal - Generalization of the basic Bicriterial controller

- Generalization to the class of MIMO state space systems with random variables described by an arbitrary probability density functions (pdf's)
- Appropriate design of the criteria
- Usage of the Gaussian sum method for estimation and employment of its multiple linearization to the dual controller
- Analysis of the Bicriterial dual controller with multiple linearization

Consider the MIMO stochastic system

$$\begin{aligned} s_{k+1} &= \mathbf{A}(\boldsymbol{\theta}_k) s_k + \mathbf{B}(\boldsymbol{\theta}_k) \mathbf{u}_k + \mathbf{w}_k, \\ \boldsymbol{\theta}_{k+1} &= \boldsymbol{\Phi}_k \boldsymbol{\theta}_k + \boldsymbol{\epsilon}_k, \\ \mathbf{y}_k &= \mathbf{C} s_k + \mathbf{v}_k, \end{aligned} \quad k = 0, \dots, N - 1$$

$s_k \in \mathbb{R}^n$... non-measurable state
 $\boldsymbol{\theta}_k \in \mathbb{R}^p$... unknown parameters
 $\mathbf{u}_k \in \mathbb{R}^r$... control
 $\mathbf{y}_k \in \mathbb{R}^m$... measurement

- ✓ The elements of matrices $\mathbf{A}(\boldsymbol{\theta}_k)$ and $\mathbf{B}(\boldsymbol{\theta}_k)$ are known linear function of the unknown parameters $\boldsymbol{\theta}_k$
- ✓ The random variables s_0 , $\boldsymbol{\theta}_0$, \mathbf{w}_k , $\boldsymbol{\epsilon}_k$ and \mathbf{v}_k are described by known pdf's

The criteria

The control objective criterion

$$J_k^c(\mathbf{u}_k) = E \left\{ (\mathbf{y}_{k+1} - \bar{\mathbf{y}}_{k+1})^T \mathbf{V}_{k+1} (\mathbf{y}_{k+1} - \bar{\mathbf{y}}_{k+1}) + \mathbf{u}_k^T \mathbf{W}_k \mathbf{u}_k \mid \mathcal{I}_k \right\}$$

$$\mathbf{u}_k^c = \underset{\mathbf{u}_k}{\operatorname{argmin}} J_k^c(\mathbf{u}_k)$$

The estimation objective criterion

$$J_k^e(\mathbf{u}_k) = E \left\{ (\mathbf{y}_{k+1} - \hat{\mathbf{y}}_{k+1})^T \mathbf{V}_{k+1} (\mathbf{y}_{k+1} - \hat{\mathbf{y}}_{k+1}) \mid \mathcal{I}_k \right\}$$

$$\mathbf{u}_k^* = \underset{\mathbf{u}_k \in \Omega_k}{\operatorname{argmax}} J_k^e(\mathbf{u}_k)$$

$$\Omega_k = [\mathbf{u}_k^c - \delta_k, \mathbf{u}_k^c + \delta_k]$$

$$\delta_k = f(\mathbf{P}_k) = \eta \cdot \operatorname{tr} \mathbf{P}_k$$

Bicriterial control law for considered MIMO system

- Structure of the control law

$$\begin{aligned} \mathbf{u}_k^* &= \mathbf{u}_k^c + \delta_k \text{sign}(\boldsymbol{\omega}_k) \\ \boldsymbol{\omega}_k &= J_k^e(\mathbf{u}_k^c + \delta_k) - J_k^e(\mathbf{u}_k^c - \delta_k) \end{aligned}$$

- Denote $\boldsymbol{\alpha}_k$, $\boldsymbol{\beta}_k$ and $\boldsymbol{\gamma}_k$ as the first, the second and the third moment of the augmented state $\mathbf{x}_k \triangleq (s_k, \boldsymbol{\theta}_k)^T$ given by the pdf $p(\mathbf{x}_k | \mathbf{y}_0^k)$, respectively. After the control law derivation the dependency of the cautious and the probing part can be written as

$$\begin{aligned} \mathbf{u}_k^c &= f(\boldsymbol{\alpha}_k, \boldsymbol{\beta}_k) \\ \boldsymbol{\omega}_k &= f(\boldsymbol{\beta}_k, \boldsymbol{\gamma}_k) \end{aligned}$$

Estimation

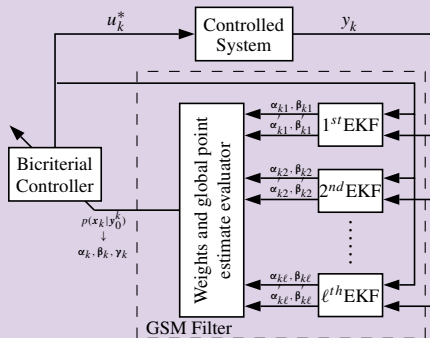
- To generate the \mathbf{u}_k^* , it is necessary to know the filtering pdf $p(\mathbf{x}_k | \mathbf{y}_0^k)$ (the system is **nonlinear system** from the estimation point of view)
- A suitable nonlinear filtering method has to be employed
- Non-Gaussian random variables \Rightarrow usage of a **global filtering method** would be advantageous

Employment of global nonlinear filtering method

The Gaussian sum method was employed

$$p(\mathbf{x}_k | y_0^k) = \sum_{i=1}^{\ell} \alpha_i \mathcal{N}(\hat{\mathbf{x}}_{ki}, \text{cov } \mathbf{x}_{ki})$$

Scheme of the Bicriterial controller



Two aspects of Bicriterial controller design

- ✓ The GSM filter is a bank of local Extended Kalman filters (EKF) which generates **local** point estimates (given by α_{ki} , β_{ki} and γ_{ki} , $\forall i$)
- ✓ The controller makes use of the **global** point estimate given by moments α_k , β_k and γ_k

⇒ Would it possible to take advantage of the local estimates?

Proposal – make use of local estimates in order to generate a probing signal that could support the estimation better

Bicriterial controller with multiple linearization

The i -th bicriterial controller coupled with the i -th EKF

$$\mathbf{u}_{ki}^* = \operatorname{argmax}_{\mathbf{u}_{ki} \in \Omega_{ki}} J_k^e(\mathbf{u}_{ki}), \quad \Omega_{ki} = [\mathbf{u}_{ki}^c - \delta_{ki}, \mathbf{u}_{ki}^c + \delta_{ki}], \quad \delta_k = \eta \operatorname{tr} \mathbf{P}_{ki}$$

$$\mathbf{u}_{ki}^* = \mathbf{u}_{ki}^c + \delta_{ki} \operatorname{sign}(\boldsymbol{\omega}_{ki}), \quad \boldsymbol{\omega}_{ki} = J_k^e(\mathbf{u}_{ki}^c + \delta_{ki}) - J_k^e(\mathbf{u}_{ki}^c - \delta_{ki})$$

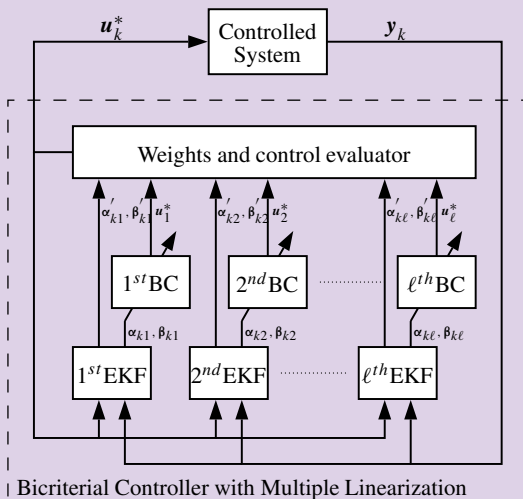
$$\mathbf{u}_k^* = \sum_{i=1}^{\ell} \alpha_i \mathbf{u}_{ki}^* = \mathbf{u}_k^c + \sum_{i=1}^{\ell} \alpha_i \delta_{ki} \operatorname{sign}(\boldsymbol{\omega}_{ki})$$

Does the controller induce different probing signal?

$$\delta_k \operatorname{sign}(\boldsymbol{\omega}_k) \stackrel{?}{\neq} \sum_{i=1}^{\ell} \alpha_i \delta_{ki} \operatorname{sign}(\boldsymbol{\omega}_{ki}).$$

Bicriterial controller with multiple linearization

Scheme of the Bicriterial controller with multiple linearization



Numerical example

Considered system

$$\begin{aligned} s_{k+1} &= \begin{pmatrix} 0 & 1 \\ \theta_1 & \theta_2 \end{pmatrix} s_k + \begin{pmatrix} \theta_3 \\ \theta_{4k} \end{pmatrix} u_k + w_k \\ \theta_{4k+1} &= \theta_{4k} + \epsilon_k \\ y_k &= (1, 1)s_k + v_k \end{aligned}$$

✓ Prior pdf of the state and the parameters

➤ $p(s_0) = \mathcal{N}((0, 0)^T, 5 \cdot \mathbf{I})$

➤ $p(\theta_0) = \mathcal{N}(\hat{\theta}_0, \text{diag}(0.8, 0.8, 1.3, 1.3)),$

$\hat{\theta}_0 = (-2.0427, 0.3427, 0, 1)^T$

✓ Noise pdf's

➤ $p(w_k) = \mathcal{N}((0, 0)^T, 10^{-4} \mathbf{I})$

➤ $p(v_k) = \mathcal{N}(0, 10^{-3})$

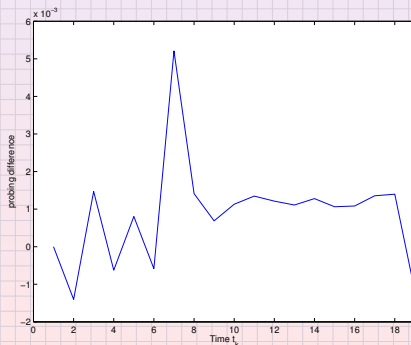
➤ $p(\epsilon_k) \sim \mathcal{U}(-0.1, 0.1)$ approximated by a Gaussian mixture with term number $\ell = 5$

✓ Probing parameter $\eta = .58$

Q: Does the inequality of probing signals hold?

⇒ The probing signals indeed differ!

$$\delta_k \text{ sign}(\omega_k) \neq \sum_{i=1}^{\ell} \alpha_i \delta_{ki} \text{ sign}(\omega_{ki}).$$



Comparison to other controllers

The following index is chosen as a measure of the control performance

$$\mathcal{M} = \sqrt{\frac{1}{N} \sum_{k=1}^N (y_k - \bar{y}_k)^2},$$

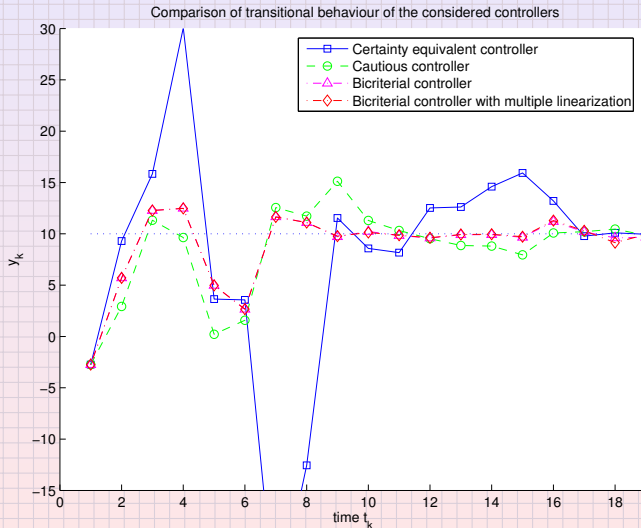
- ✓ y_k represents the measurement
- ✓ \bar{y}_k represents the reference value
- ✓ N determines length of one simulation run

The expected value $\hat{\mathcal{M}} = E \{ \mathcal{M} \}$ is estimated using 5000 Monte Carlo simulations.

Control quality comparison using the index $\hat{\mathcal{M}}$

	$\hat{\mathcal{M}}$
Certainty equivalent controller	9.9212
Cautious controller	4.9824
Bicriterial controller	4.8634
Bicriterial controller with multiple linearization	4.8578

Comparison to other controllers



Concluding remarks

- Generalization of the Bicriterial dual controller was presented
- Some aspects of Bicriterial controller were discussed
- Bicriterial control scheme employing multiple linearization was suggested
- The cautious part of the multiple linearized control law is unchanged
- The two Bicriterial controller schemes induces different probing signal